Application of Modified Derived Equations of Motion of Respiratory Mechanics in the Interpretation of Ventilator Graphics

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Abstract: Ventilator Graphics is an indispensable tool at the bedside for monitoring of the mechanical ventilation. The basic mathematical models of breathing mechanics consider the respiratory system as a single compartment model relating the pressure, volume, and flow during Ventilation. This is known as the Equation of Motion for the respiratory system or the force balance equation. The understanding and application of these concepts play a vital role in the intensive care unit patients. Amid the COVID-19 critical situation, the Ventilators play a major role in the management of these patients. Although continuous advancement in Mechanical Ventilator technology takes place, understanding and interpretation of Ventilator Graphics at the bedside is considered the most important part in management of critically ill patients. In the current study, newer equations are derived by modifying the equations of motion of the respiratory mechanics and the application of these research findings are summarized. The study concludes that the application of these novel equations which are to be considered as differential equations may help in better understanding of the mechanical ventilation that helps in the interpretation of invaluable ventilator graphics.

Keywords: Respiratory Mechanics, Mathematical Model, Modified Derived Equation of Motion

1. INTRODUCTION

Ventilator Graphics is an indispensable tool at the bedside for monitoring of the mechanical ventilation. Amid the COVID-19 critical situation, the Ventilators play a major role in the management of these patients. Although continuous advancement in Mechanical Ventilator technology takes place, understanding and interpretation of Ventilator Graphics at the bedside is considered the most important in management of intensive care unit (ICU) patients.[I] The basic mathematical model of breathing mechanics consider the respiratory system as a single compartment model relating the pressure, volume, and flow during Ventilation. This is known as the Equation of Motion for the respiratory system or the force balance equation.[II, III] The movement of air takes place between atmosphere and the alveoli inside the lungs during breathing. This movement is driven by the pressure gradient between these two sites and hindered by the presence of airway resistance. The amount of air flow through an airway in a given period of time depends on this pressure gradient and the airway resistance.[III]

Inhalation is an active process that requires resistive work of breathing to overcome the frictional resistance to flow and elastic work of breathing to overcome the elastance (reciprocal of compliance) of the respiratory system. This can be compared to the pressure needed to inflate a balloon through a straw where the pressure is needed to overcome both the resistance of the straw and elasticity of the balloon.[III] The energy required for inspiration is more than that required for expiration under physiological conditions because only resistive work of breathing is required for expiration. Tidal breathing during exhalation is a passive process that does not require active energy. The elastic energy stored during inspiration is partly utilized as resistive work of breathing for expiration and partly dissipated as heat energy.[IV] The pressure required for expiratory flow to exhale the necessary tidal
A ventilator mode refers to the set of operating characteristics that control how the ventilator functions. It indicates the pattern of breath delivery and how the breaths are triggered, cycled and limited. If the inspiration is both triggered (started) and cycled (stopped) by the patient, then it is called as spontaneous breath. If the inspiration is either ventilator triggered or ventilator cycled or both, then it is called as mandatory breath. The spontaneous breaths may be assisted or unassisted. An assisted breath is a breath during which all or part of inspiratory (or expiratory) flow is generated by the ventilator doing work on the patient. The total cycle time (TCT) or Ventilator period denotes the sum of both inspiratory time and expiratory time and it is inversely related to frequency. Minute ventilation is the tidal volume times the respiratory rate (frequency).

The time constant characterizes the rate of variation of the function over a period of time. Time constant is relevant when modelling a process using exponential functions and it does not apply for constant functions. During inspiration, the time constant can only be evaluated in the pressure controlled ventilations because the inspiratory flow time waveform will be in the exponential form. During exhalation, the time constant can be evaluated regardless of the ventilation mode because the expiratory flow time waveform is an exponential function for passive expiration. So, the Expiratory time constant is very useful for assessing the overall respiratory mechanics.
The inspiratory time \((T_I)\) is to be represented in terms of inspiratory time constant \((\tau_i\) or \(RC_{ins}\)) and similarly expiratory time \((T_E)\) is to be represented in units of expiratory time constant \((\tau_e\) or \(RC_{exp}\)). Their calculated ratios namely \(T_i/RC_{ins}\) and \(T_E/RC_{exp}\) are used to assess the completion of the process of inspiration and expiration. A ratio of 5, 4, 3, 2, and 1 denotes a completion of the process of 99.3%, 98.2%, 95.1%, 86.5%, and 63.3% respectively. The inspiration process will increase by these percentages and the expiration process will decrease by these percentages (clearly shown in figure 1).[VI,XIV]

Figure 1. Time Constant for Exponential Functions

The time constant measured in seconds is calculated using the product of resistance \((R)\) and compliance \((C)\). Inspiratory time constant \((RC_{ins})\) and expiratory time constant \((RC_{exp})\) are not equal because of lower airway resistance during inspiration. Thus inspiratory time constant is shorter than the expiratory time constant.[II,VI,XVI]

Time constant (in seconds) = Resistance x Compliance

\[
RC_{ins} = C_{stat} \times R_{ins} \quad & \quad RC_{exp} = C_{stat} \times R_{exp}
\]

3. EQUATION OF MOTION OF RESPIRATORY SYSTEM

The Equation of motion of Respiratory system of respiratory mechanics or Force balance equation which is given below is also a differential equation.[II] Pressure as a function of time \(P(t)\) is related to the volume and flow with constant coefficients (elastance and resistance).

\[
P(t) = R.[dv/dt] + E.v(t)
\]

The volume as a function of time represented by \(v(t)\) is equal to the constant (or average) flow multiplied by time. The flow is calculated using the derivative of volume \(v(t)\) with respect to time \(t\) which is denoted by \(dv/dt\).[2]Volume curve is usually not measured directly but it is derived from the flow measurement as the area under the flow time curve using integral calculus.[II,XVI] The Equation of motion of respiratory mechanics in simplified form is given below.

\[
P_{AW} = Flow \times Resistance + Elastance \times Tidal \ Volume
\]

\[
P_{AW} = F \times R + E \times TV
\]

\[
P_{AW} = P_{RES} + P_{EL}
\]

\[
P_{RES} = F \times R \quad ; \quad P_{EL} = E \times TV
\]

Where \(P_{AW}\) is the pressure generated either by the ventilator or the muscle.

4. DERIVATIONS OF EQUATIONS OF MOTION

At any moment during inspiration, the airway pressure must exactly balance the forces opposing lung and chest wall expansion. The opposing pressures are the sum of flow resistive pressure \(P_{RES}\), elastic recoil pressure \(P_{EL}\) and inertia pressure \(P_{inertance}\) of the respiratory system.[III, XIII,XIV]
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\[ P_{AW} = P_{RES} + P_{EL} + P_{\text{inertance}} \]

The inertial forces are usually negligible during conventional ventilation. The inertance pressure\( (P_{\text{inertance}}) \) of the respiratory system can be omitted from the equation and the equation of motion is simplified as given below.

\[ P_{AW} = P_{RES} + P_{EL} \]

In the presence of positive end expiratory pressure\( (PEEP) \), the equation of motion of the respiratory system is written as follows.

\[ P_{AW} = P_{RES} + P_{EL} + P_{\text{PEEP}} \]

The ventilator will generate a positive pressure and the gas will flow from higher to lower pressure. The muscle will generate a negative pressure at the other end so the gas will flow through the pressure gradient.[XVII] So the above equation can be written as follows using the pressure generated by the ventilator and the muscle.

\[ P_{\text{VENT}} = P_{RES} + P_{EL} - P_{\text{MUS}} + P_{\text{PEEP}} \]

The equation contains \( P_{\text{MUS}} \) with negative sign because it acts by creating a negative pressure at the other end. The equation can be re-written in the following form.

\[ P_{\text{VENT}} + P_{\text{MUS}} = P_{RES} + P_{EL} + P_{\text{PEEP}} \]

\[ P_{AW} = P_{RES} + P_{EL} + P_{\text{PEEP}} \]

\[ \Delta P = P_{RES} + P_{EL} \quad \text{where} \quad \Delta P = P_{AW} - P_{\text{PEEP}} \]

\( P_{AW} \) is the pressure generated either by the ventilator or the muscle. From this equation it is very clear that the pressure generated by the ventilator and/or muscle has to increase above the PEEP level for the pressure gradient to develop that helps in flow of gas across the respiratory system.[II]

5. **Auto PEEP**

Auto PEEP is present if flow does not reach zero before the beginning of inspiration. Flow waveform can identify it, but it cannot quantify the value of auto PEEP.[II,XVI] It is clearly depicted in the figure 2 using the flow time waveform. The pressure generated due to the volume of this trapped air \( (V_{\text{trap}}) \) is the product of elastance and residual volume.

Auto PEEP = \( V_{\text{trap}} \times E \)

Auto PEEP is the product of Expiratory Resistance and Residual Flow\( (rF) \).[II]

Auto PEEP = \( R \times rF \)

Total PEEP = Auto PEEP + Set PEEP

Total PEEP = \( R \times rF + \text{Set PEEP} \)

![Figure2. Air Trapping - Flow Time Waveform](image)
6. **NEWLY MODIFIED DERIVED EQUATIONS OF MOTION**

Let the End expiratory alveolar volume be denoted by \( V \) and the amount of tidal volume inspired during inhalation be denoted by \( \Delta V \). Then \([V + \Delta V]\) denote End inspiratory alveolar volume. Let the amount of tidal volume expired during exhalation be denoted by \( dV \). If the amount of tidal volume inhaled(\( \Delta V \)) and the amount of tidal volume exhaled(\( dV \)) are equal then the difference between these values will be zero. But under certain conditions, these volumes may differ and their difference will increase. Decreased expiratory flow increases the residual volume that results in air trapping which may lead to a decreased exhaled tidal volume. If there is leakage then exhaled tidal volume will be grossly lower than the amount of inhaled tidal volume. [II,XVI]

7. **DERIVATION OF INSPIRATORY FLOW WITH PRESSURE GRADIENT, ELASTANCE AND RESISTANCE**

\[ P_{AW} - PEEP = P_{RES} + P_{EL} \]

Inspiration is an active process that needs energy for both resistive and elastic work. The resistive pressure gradient depends on the product of flow and resistance(\( R \)) and the elastic pressure gradient depends on the product of elastance(\( E \)) and the amount of tidal volume (TV) inhaled.[II,III,IV]

\[ P_{AW} - PEEP = iF \times R + E \times TV \]

For constant flow, Tidal Volume is the product of Inspiratory Flow (\( iF \)) and Inspiratory Time(\( Ti \)). Auto PEEP is the product of Resistance and Residual Flow(\( rF \)).[II]

\[ P_{AW} - PEEP = iF \times R + E \times TV \] \( \text{Where } TV = iF \times Ti \)

\[ P_{AW} - PEEP = iF(R + ExtI) \]

\[ \text{Where Total PEEP = R x rF + Set PEEP} \]

\[ P_{AW} - Set PEEP - R x rF = iF(R + ExtI) \]

\[ \Delta P = iF(R + ExtI) + R x rF \]

In the absence of Auto PEEP,

\[ \Delta P = iF(R + ExtI) \] \( \text{Where } \Delta P = P_{AW} - Set PEEP \)

8. **DERIVATION OF INSPIRATORY FLOW WITH COMPLIANCE(C) AND TIME CONSTANT**

\[ \Delta P = iF(R + ExtI) + R x rF \]

\[ \Delta P = R x rF = iF(R + ExtI) \] \( \text{Where } E = 1/C \)

\[ \Delta P = R x rF = [iF/C] \times (RC + Ti) \]

\[ \Delta P = R x rF = [iF/C] \times (\tau_i + Ti) \]

\[ iF = \left(\frac{\Delta P - R x rF}{C}\right) / (\tau_i + Ti) \]

In the absence of Auto PEEP, **residual flow** is zero. So, the above equation becomes,

\[ iF = \frac{\Delta P \times C}{(\tau_i + Ti)} \]

9. **DERIVATION OF INSPIRATORY FLOW WITH RESISTANCE AND PRESSURE GRADIENT**

\[ P_{AW} - PEEP = iF \times R + E \times TV \]

\[ iF \times R + E \times TV = P_{AW} - PEEP \]

\[ iF \times R + E \times TV = P_{AW} - Set PEEP - R x rF \]

\[ iF \times R = P_{AW} - Set PEEP - R x rF - E \times TV \]

\[ iF \times R = P_{AW} - Set PEEP - (R x rF + E \times TV) \]
Let the amount of tidal volume inspired during inhalation be denoted by $\Delta V$. The above equation can written as follows.

$$iF = \left[\frac{1}{R}\right] \times \left\{ \Delta P - (R \times rF + E \times \Delta V) \right\}$$ ; Where $\Delta P = P_{AW} - \text{Set PEEP}$

In the absence of Auto PEEP, residual flow is zero. So, the above equation is reduced to the following equation.

$$iF = \left[\frac{1}{R}\right] \times \left\{ \Delta P - E \times \Delta V \right\}$$

### 10. Derivation of Expiratory Flow with Resistance and Pressure Gradient

Expiration is a process that needs energy only for the resistive work which is provided by the elastic energy stored during inspiration.[IV] End expiratory alveolar pressure is the product of End expiratory alveolar volume(V) and elastance(E). End inspiratory alveolar pressure is the product of End inspiratory alveolar volume $[V + \Delta V]$ and elastance(E). The required passive elastic recoil pressure ($P_{EL}$) is calculated as the difference between End inspiratory alveolar pressure and End expiratory alveolar pressure.

$$P_{EL} = [V + \Delta V] \times E - [V \times E]$$

$$P_{EL} = E \times [V + \Delta V - V]$$

$$P_{EL} = E \times \Delta V$$

$\Delta V$ - denote the amount of inhaled tidal volume

The Equation of Motion of the Respiratory System for Expiration is as follows.[II]

$$P_{VENT} + P_{MUS} = P_{RES} + P_{EL}$$

For Expiration: $P_{VENT}$ & $P_{MUS}$ are zero.

$$P_{EL} = - (P_{RES})$$

$$E \times \Delta V = - R \times eF$$

The energy for the expiratory resistive work is provided by the elastic energy stored during the inspired tidal volume.[IV] The Equation of Motion of the Respiratory System for Expiration with PEEP is as follows.[II]

$$P_{VENT} + P_{MUS} = P_{RES} + P_{EL} + \text{PEEP}$$

For Expiration: $P_{VENT}$ & $P_{MUS}$ are zero.

$$P_{EL} = - (P_{RES} + \text{PEEP})$$

At each moment in time, the pressure necessary to cause expiratory flow is equal to the pressure stored in the lungs due to elastic recoil. The negative sign indicates flow during expiration is in the opposite direction of inspiration.[II] Negative sign can be omitted to compare only the magnitude of the pressure.

$$E \times \Delta V = (R \times eF + \text{PEEP})$$

$$R \times eF = E \times \Delta V - \text{PEEP}$$

$$R \times eF = E \times \Delta V - \text{Auto PEEP} - \text{Set PEEP}$$

$$R \times eF = E \times \Delta V - R \times rF - \text{Set PEEP}$$

$$R \times eF + R \times rF = E \times \Delta V - \text{Set PEEP}$$

$$R \times [eF + rF] = E \times \Delta V - \text{Set PEEP}$$

$$[eF + rF] = [1/R] \times \left\{ E \times \Delta V - \text{Set PEEP} \right\}$$
In the absence of Auto PEEP, residual flow is zero. So, the above equation becomes the following.
\[ eF = \left[ \frac{1}{R} \right] \times \left( E \times \Delta V - \text{Set PEEP} \right) \]

It is very clear from the above relation that the expiratory flow is driven by the gradient between alveolar pressure and set PEEP and decreased by resistance.

11. **DERIVATION OF END EXPIRATORY ALVEOLAR PRESSURE, PEEP & AUTO PEEP**

The pressure necessary to cause expiratory flow is equal to the pressure stored in the lungs due to elastic recoil [II,IV]
\[ E \times \Delta V = (R \times eF + \text{PEEP}) \]
\[ E \times \Delta V = (R \times eF + \text{Auto PEEP} + \text{Set PEEP}) \]

The expiratory hold pause the breath in expiration. The expiratory flow is interrupted by preventing the next breath to happen. With the flow stopped, the flow goes to zero the alveolar pressure equilibrates with the ventilator circuit. If some air remains trapped then the residual pressure in the lungs equilibrates with the patient circuit [II,XIV,XVI,XVIII]
\[ E \times \Delta V = (R \times eF + \text{Auto PEEP} + \text{Set PEEP}) \]
\[ E \times \Delta V - R \times eF = \text{Auto PEEP} + \text{Set PEEP} \]

At the end of expiration, expiratory flow (eF) is zero and Volume will be the resting volume because the tidal volume is exhaled, so \( \Delta V \) changes to \( V \).
\[ \Delta V: \text{Tidal Volume inhaled} \]
\[ V: \text{End expiratory alveolar volume} \]

So, the above equation is changed to the following equation.
\[ E \times V = (\text{Auto PEEP} + \text{Set PEEP}) \]
\[ \text{Auto PEEP} = E \times V - \text{Set PEEP} \]

**AUTO PEEP** (also known as intrinsic or occult PEEP) is the positive difference between end expiratory alveolar pressure and the end expiratory airway pressure (PEEP set by the clinician). Total end expiratory pressure is the sum of the auto-PEEP and the extrinsically applied PEEP in the mechanically ventilated patient [II,XIV,XVI,XVIII]  
\[ \text{Auto PEEP} = E \times V - \text{Set PEEP} \]

In the absence of auto PEEP, the above equation changes to the following.
\[ E \times V = \text{Set PEEP} ; V = C \times \text{Set PEEP} \]
\[ E \times V = (\text{Auto PEEP} + \text{Set PEEP}) \]

From the above relation it is very clear that end expiratory alveolar pressure and volume depends on set PEEP and Auto PEEP. The set PEEP increases the volume by both distension of previously open alveoli and recruitment of alveoli [XIX,XX]

12. **DERIVATION OF EXPIRATORY TIME CONSTANT (\( \tau_e \))**

The pressure necessary to cause expiratory flow in the presence of auto PEEP is as follows.
\[ E \times \Delta V = (R \times eF + \text{Auto PEEP} + \text{Set PEEP}) \]
\[ E \times \Delta V = (R \times eF + E \times V) ; \text{Where } E \times V = (\text{Auto PEEP} + \text{Set PEEP}) \]
\[ E \times (\Delta V - V) = R \times eF \]
\[ (\Delta V - V) = R \times C \times eF ; \text{ Where } E = 1/C \text{ and } \tau_e = RC \]
\[ \tau_e = \frac{[\Delta V - V]}{eF} \]

OR
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\[ E \times \Delta V = (R \times eF + \text{Auto PEEP} + E \times V); \text{ Where } E \times V = \text{Set PEEP} \]

\[ E \times \Delta V = (R \times eF + R \times rF + E \times V) \]

\[ E \times (\Delta V - V) = R \times (eF + rF) \]

\[ (\Delta V - V) = R \times (eF + rF) \]

\[ \tau_e = \frac{[\Delta V - V]}{(eF + rF)} \]

If the residual flow is zero,

\[ \tau_e = \frac{[\Delta V - V]}{eF} \]

In the absence of auto PEEP, expiratory time constant is the ratio between the exhaled tidal volume and the peak expiratory flow.

V: End expiratory alveolar volume

\( \Delta V \): Amount of tidal volume inspired

\( [V + \Delta V] \): End inspiratory alveolar volume

\( [\Delta V - V] \): Exhaled Tidal Volume

During inspiration the lung volume increases by the amount of inhaled tidal volume(\( \Delta V \)) and then during expiration the lung volume decreases, reaching the resting volume by the exhaled tidal volume(\( dV \)) at the end of expiration.

\[ \Delta V - dV = V \quad \text{OR} \quad \Delta V - V = dV \]

The difference between the Inhaled Tidal Volume and the Exhaled Tidal Volume will be the normal resting lung volume. It is very clear that Increased Resting Lung Volume results if the exhaled tidal volume is lower than the inhaled tidal volume.

13. **TOTAL WORK DONE DURING INSPIRATION**

Total pressure required to inflate the lung is the sum of the pressure required to overcome the airway resistance and the elastance of the respiratory system.[II,III,IV]

\[ P_{AW} - \text{Set PEEP} = iF(R + EXTi) + R \times rF \]

The above relation shows that the pressure gradient increased above set PEEP, is necessary for the inspiratory flow. The work required to deliver a tidal breath during inspiration is the product of tidal volume(\( TV \)) and airway Pressure.[II,XIV]

Work done = pressure X Change in volume

\[ W_{TOT} = \{ iF(R + EXTi) + R \times rF \} \times TV \]

The above equation represents the total work done to overcome the resistive and elastic elements of the respiratory system.[VIII] Also the work done is increased in the presence of auto PEEP generated by the product of residual flow and resistance.

14. **WORK DONE DURING EXPIRATION BY PASSIVE ELASTIC RECOIL PRESSURE**

Work done during inhalation is stored as potential energy which is recovered during exhalation. Elastic energy due to the elastic recoil of the lung is stored as potential energy which provides the necessary pressure required for exhaling the tidal volume.[IV] The pressure necessary to cause expiratory flow in the presence of auto PEEP is as follows.

\[ \{E \times \Delta V - \text{Set PEEP}\} = R \times (eF + rF) \]

\[ P_{EL} - \text{Set PEEP} = R \times (eF + rF) \]

Work done = pressure X Change in volume

\[ W_{EL} = R \times (eF + rF) \times dV \]
The work required to exhale a tidal volume during expiration is the product of amount of tidal Volume exhaled (dV) and the passive elastic recoil pressure gradient. The work done during breathing is increased by the resistance which is shown in the figure 3 using the pressure volume work during the inspiration and expiration.

**Figure 3. Increased Work of Breathing**

**15. RESULTS**

The novel derived modified equations of motion of respiratory mechanics (five equations) are tabulated in table 1. The Passive Elastic Recoil Pressure (P_{EL}), End Expiratory Alveolar Pressure, work done during inspiration and work done by the passive elastic recoil of lung during expiration are tabulated in table 2. These equations are represented in two forms, one in the presence of auto PEEP and other in the absence of auto PEEP. These are to be considered as differential equations and not as algebraic equations.

**Table 1: Novel Derived Modified Equations of Motion**

<table>
<thead>
<tr>
<th>S.NO</th>
<th>PARAMETER</th>
<th>FORMULAE</th>
</tr>
</thead>
<tbody>
<tr>
<td>1</td>
<td>( \Delta P ):</td>
<td>( \Delta P = iF(R + EXT_i) + R x rF ) \hspace{1cm} ( \Delta P = iF(R + EXT_i) )</td>
</tr>
<tr>
<td>2</td>
<td>( iF ): Inspiratory Flow with compliance, Inspiratory time constant and Inspiratory time</td>
<td>( iF = \left( \frac{\Delta P - R x rF}{C} \right) \div (\tau_i + Ti) ) \hspace{1cm} ( iF = \frac{\Delta P}{C} \div (\tau_i + Ti) )</td>
</tr>
<tr>
<td>3</td>
<td>( eF ): Expiratory Flow with Pressure Gradient and resistance</td>
<td>( eF = \left( \frac{\Delta P - E X \Delta V}{E X \Delta V} \right) ) \hspace{1cm} ( eF = \left( \frac{\Delta P - E X \Delta V}{E X \Delta V} \right) )</td>
</tr>
<tr>
<td>4</td>
<td>( \tau_e ): Expiratory Time Constant</td>
<td>( \tau_e = \frac{\Delta V - V}{eF + rF} ) \hspace{1cm} ( \tau_e = \frac{\Delta V - V}{eF} )</td>
</tr>
</tbody>
</table>
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Table 2. Passive Elastic Recoil Pressure & Work Done

<table>
<thead>
<tr>
<th>S.NO</th>
<th>PARAMETER</th>
<th>FORMULAE</th>
</tr>
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<tbody>
<tr>
<td></td>
<td>In the Presence of AutoPEEP (Above)</td>
<td></td>
</tr>
<tr>
<td></td>
<td>In the Absence of AutoPEEP (Below)</td>
<td></td>
</tr>
<tr>
<td>6</td>
<td>( \text{E X } \Delta V : ) Passive Elastic Recoil Pressure ((P_{EL}))</td>
<td>(\text{E X } \Delta V = (R \times \text{eF} + \text{Auto PEEP} + \text{Set PEEP}))</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(\text{E X } \Delta V = (R \times \text{eF} + \text{Set PEEP}))</td>
</tr>
<tr>
<td>7</td>
<td>( \text{E X V :} ) End Expiratory Alveolar Pressure</td>
<td>(\text{E X V} = \text{Auto PEEP} + \text{Set PEEP})</td>
</tr>
<tr>
<td></td>
<td></td>
<td>(\text{E X V} = \text{Set PEEP})</td>
</tr>
<tr>
<td>8</td>
<td>( \text{W}_{\text{TOT}}: ) Total Work done During Active Inspiration</td>
<td>(\text{W}_{\text{TOT}} = { \text{iF}(R + \text{EXTi}) + R \times \text{rF} } \times \Delta V)</td>
</tr>
<tr>
<td>9</td>
<td>( \text{W}_{\text{EL}}: ) Work done During Passive Expiration by the Elastic Recoil Pressure</td>
<td>(\text{W}_{\text{EL}} = R \times (\text{eF} + \text{rF}) \times dV)</td>
</tr>
</tbody>
</table>

16. DISCUSSION

Ventilators play a major role in the management of intensive care unit patients. Ventilator Graphical tool helps in monitoring the mechanical ventilation at the bedside. A lot of advancement in Mechanical Ventilator technology has taken place yet the understanding and interpretation of Ventilator Graphics at the bedside seems to be a challenging one. [I] The Equation of Motion for the respiratory system is the basic mathematical model of breathing mechanics. [II] The understanding and application of the various physical concepts involved in it plays a vital role in the management of these patients.

17. APPLICATION OF THE NEWLY DERIVED MODIFIED EQUATIONS

The application of the derived modified equations of motion of the respiratory system of the respiratory mechanics is to be discussed in detail. Total Work done during the inspiration includes both resistive and elastic work. It is decreased by the compliance, increased by the inspiratory resistance, elastance and the auto PEEP generated due to the residual flow. The pressure gradient required for the inspiratory flow is decreased by the set PEEP and increased by the resistance at the start of inspiration.

\[
\Delta P = \text{iF}(R + \text{EXTi}) + R \times \text{rF} ; \quad \text{Where } \Delta P = P_{\text{AW}} - \text{set PEEP}
\]

In the presence of auto PEEP, the pressure gradient required for causing the flow will be higher. But in the absence of Auto PEEP, residual flow is zero and so the above equation is reduced to the following form.

\[
\Delta P = \text{iF}(R + \text{EXTi})
\]

\[
\Delta P = \text{iF}(R + \text{EX0}) ; \quad \text{At time } T_i = \text{zero}
\]

\[
\Delta P = \text{iF} \times R \quad \text{OR} \quad \text{iF} = \Delta P/R
\]

If the resistance is increased then the Peak inspiratory flow will decrease. In constant flow mode of ventilation, peak inspiratory flow rate is seen at the beginning of the inspiratory cycle depending on the set inspiratory rise time (normal, too fast and too slow) in the ventilator, then the inspiratory flow is constant throughout the inspiratory cycle and it ceases once the preset or target value is achieved. The inspiratory rise time determines the amount of time it takes to reach the desired airway pressure or peak flow rate (shown in figure 4). [XV] It determines the rate at which the ventilator achieves a target pressure in pressure control and pressure support modes or flow rate in volume control modes.
Figure 4. Normal Inspiratory Rise Time

During the initial portion of inspiration, the pressure gradient is a function of flow and resistance. Thus the pressure time waveform in the constant flow mode of ventilation begins with an exponential rise to a first step. If the resistance is higher, then the rise in step will be much higher (figure 5 A). The second portion of the pressure time waveform is a linear increase to peak inspiratory pressure (PIP) representing the peak dynamic pressure that includes both the resistive and elastic components. [XIV, XVI, XVIII] As the inspiratory time Ti increases, the term (R + Ex Ti) will increase. The second portion of the pressure time waveform depends mainly on the elastance which is the reciprocal of compliance. If the compliance is decreased, then the elastance is increased and so the slope of the second portion is increased (figure 5 B).

\[ IF = \frac{[\Delta P - R \times rF] \times C}{(\tau_i + Ti)} \]

Higher pressure gradient is required for causing the inspiratory flow in the presence of auto PEEP. The residual flow is zero in the absence of Auto PEEP and so, the above equation is reduced to become the following equation.

\[ iF = \frac{[\Delta P \times C]}{(\tau_i + Ti)} \]
In constant pressure mode of ventilation, the Inspiratory flow is directly proportional to the pressure gradient (driving force) and the compliance and inversely proportional to the Inspiratory Time Constant. The peak inspiratory flow is seen at the start of inspiration (depending on the set inspiratory rise time) due to maximum pressure gradient and as the Inspiratory time increases, the pressure gradient is decreased due to the inspired tidal volume, so the inspiratory flow decreases till it reaches the baseline. The inspiratory flow will be higher if the patient has increased compliance (decreased elastance) and the inspiratory flow will be lower if the patient has decreased compliance (increased elastance) as depicted in the figure 6. If the inspiratory time constant is shorter, the tidal volume is inhaled quickly or short inspiratory time is sufficient to inhale the tidal volume. If the inspiratory time constant is longer, the tidal volume is inhaled slowly or long inspiratory time is needed to inhale the required tidal volume. As the inspiratory time constant ($\tau_i$) increases, the inspiratory flow will decrease and vice versa.

**Figure 6. Decreased Compliance - Flow Time Waveform**

\[ iF = \left[ \frac{1}{R} \right] \times \left\{ \Delta P - (R \times rF + E \times \Delta V) \right\} \]

The inspiratory flow requires higher pressure gradient in the presence of auto PEEP. If the residual flow is zero (absence of Auto PEEP), the above equation is reduced to become the following equation.

\[ iF = \left[ \frac{1}{R} \right] \times \left\{ \Delta P - E \times \Delta V \right\} \]

In constant pressure mode of ventilation, the Inspiratory flow is directly proportional to the pressure gradient (driving force) and inversely proportional to the resistance. The inspiration starts at the end expiratory alveolar volume denoted by $V$. The pressure gradient at the start of inspiration is denoted by $\{\Delta P - E \times V\}$ and the pressure gradient is maximum at this starting point and so the peak inspiratory flow is always seen at the beginning of the inspiration. The pressure gradient at the end of inspiration will be denoted by $\{\Delta P - E \times \Delta V\}$ and as the tidal volume ($\Delta V$) is inhaled during inspiration, the pressure gradient $\{\Delta P - E \times \Delta V\}$ decreases and the flow ceases if the pressure gradient is zero $\{\Delta P = E \times \Delta V\}$. The inspiratory flow will decrease with increase in resistance, so more inspiratory time is needed to deliver the required volume otherwise the inspired tidal volume will be decreased as compared with normal resistance patients which is clearly depicted in the figure 7.[XIV]
Figure 7. Increased Resistance - Flow Time Waveform

The figure 7 clearly shows that in constant pressure mode of ventilation, both the inspiratory and expiratory flow will be reduced with increase in resistance but in constant flow mode of ventilation only the expiratory flow is reduced with increase in resistance because the inspiration is controlled by the ventilator.

\[ [eF + rF] = \frac{1}{R} \times \{ E \times \Delta V - \text{Set PEEP} \} \]

Expiratory flow is driven by pressure gradient between alveolar pressure and set PEEP and decreased by the resistance which are related in the above equation. If the expiratory flow is inadequate then the residual flow increases which contributes to the generation of auto PEEP. If the residual flow is zero (absence of Auto PEEP), the above equation is reduced to the following form.

\[ eF = \frac{1}{R} \times \{ E \times \Delta V - \text{Set PEEP} \} \]

Normal expiration starts with peak expiratory flow, followed by a gradual decrease in flow. [II,XIV,XV] Higher expiratory resistance (obstruction) leads to a reduced peak expiratory flow, prolonged expiratory time and the expiratory flow time curve decays slowly which are depicted in figure 8.

Figure 8. Reduce Expiratory Flow Rate - Flow Time Waveform
Let the inspired tidal volume be denoted by $\Delta V$. If the End expiratory alveolar volume is denoted by $V$, then $[V + \Delta V]$ denote the End inspiratory alveolar volume. The pressure gradient is maximum at beginning of expiration (end of inspiration) and then as the tidal volume is exhaled the pressure gradient decreases gradually. The peak expiratory flow will be seen at the beginning of the expiration and then the lung volume decreases towards the resting volume in the end of expiration.\[II,XIV,XV,XVI\] If airway obstruction is present, then the peak expiratory flow will be reduced and then it decreases very slowly towards the resting volume which is clearly noticed as scooping in the flow volume loop shown in the figure 9.

![Figure 9. Reduce Expiratory Flow Rate- Flow volume Loop](image)

The passive elastic recoil pressure ($P_{EL}$) required for causing flow during expiration is calculated as the difference between End inspiratory alveolar pressure and End expiratory alveolar pressure ($P_{EL} = E \times \Delta V$). The resistive work of expiration is provided by the elastic energy stored during inspiration.\[IV\] The pressure necessary to cause expiratory flow in the presence of auto PEEP is shown in the below equation.

$$E \times \Delta V = (R \times eF + \text{Auto PEEP} + \text{Set PEEP})$$

If the required tidal volume inhaled during inspiration is exhaled by the expiratory flow then there is no residual flow. The pressure necessary to cause expiratory flow in the absence of auto PEEP is given in the below equation.

$$E \times \Delta V = (R \times eF + \text{Set PEEP})$$

At the end of expiration, the expiratory flow ($eF$) is zero and Volume will be the resting volume because the tidal volume is exhaled. Functional Residual Capacity (FRC) is the volume of gas that remains in the lungs at the end of expiration which is the resting state and in the presence of positive end-expiration pressure (PEEP) it is called the end-expiratory lung volume (EELV). FRC is a lung volume measured without PEEP (at atmospheric pressure). PEEP contributes to increased end-expiratory lung volume (EELV) by recruitment of previously non-aerated alveolar units and distension of previously open alveolar units. If no recruitment occurs then the volume increased by the set PEEP will be the result of product of compliance and set PEEP (i.e., $C \times \text{set PEEP}$). When there is a larger change in volume, then that volume gain will be due to the recruitment.\[XIX-XXII\]

$$E \times V = (\text{Auto PEEP} + \text{Set PEEP})$$

The end expiratory alveolar pressure and volume depends on both the externally set PEEP and auto-generated PEEP. The set PEEP increases the volume by recruitment of alveoli as well as distension of previously open alveoli. If there is no auto PEEP and the set PEEP is zero, then the end expiratory alveolar pressure will be at the atmospheric pressure level.
The relationship between the expiratory time constant, expiratory flow, residual flow and the alveolar volume at the end of inspiration and expiration is given in the below equation.

\[ \tau_e = \frac{[\Delta V - V]}{(eF + rF)} \]

If the residual flow \((rF)\) is zero (absence of auto PEEP), then the above equation is reduced to the following relation.

\[ \tau_e = \frac{[\Delta V - V]}{eF} \]

- \([\Delta V]\): Inhaled Tidal Volume
- \([V + \Delta V]\): End inspiratory alveolar volume
- \(V\): End Expiratory Alveolar Volume

Expiration time constant = exhaled tidal volume / peak expiratory flow

The above simple formula is already used to calculate the expiratory time constant which is the ratio between the exhaled tidal volume and the peak expiratory flow. It treats the lung as single compartment and does not account for time constant heterogeneity of lungs.\([IX]\) In the presence of auto PEEP, the above formula is inaccurate and so it cannot be used to calculate the expiratory time constant. During inspiration the lung volume increases by the amount of inhaled tidal volume \((\Delta V)\). Then the lung volume decreases during expiration and it reaches the resting volume at the end of expiration by the exhaled tidal volume \((dV)\)

\[ \Delta V - dV = V \quad OR \quad \Delta V - V = dV \]

If the inhaled tidal volume is completely expelled by the exhaled tidal volume then the resting lung volume is normal. If the Inhaled Tidal Volume is not completely expelled by the exhaled Tidal Volume due to incomplete expiration, then the resting lung volume is increased. When the expiration time is insufficient, the expiratory flow will decrease and consequently the residual flow will increase leading to an increase in end expiratory lung volume that result in dynamic hyperinflation. This prevents the respiratory system from returning to its resting end expiratory equilibrium volume between breath cycles.\([X,XI,XII]\)

Figure 10. Air Trapping – Constant Pressure Mode of Ventilation

The figure 10 clearly shows that the expiratory flow does not reach zero which increases residual flow that result in air trapping. Trapped gas volume or residual volume refers to the gas volume associated with dynamic hyperinflation and auto PEEP. Increase of elastic recoil and decrease of airway resistance are effective to obtain higher expiratory flow. The collapse of alveoli will also result in generation of auto PEEP.\([X]\)

Auto PEEP = Dynamic hyperinflation x Elastance

Auto PEEP acts as an inspiratory load that must be counterbalanced for the inspiratory flow to begin.\([II,XIV]\) Auto PEEP could be more effectively reduced by increasing expiratory time (either
increasing inspiratory flow or reducing breathing frequency) to increase the ratio between expiratory time and time constant rather than by decreasing the inspired tidal volume.[X,XI,XII,XV] The expiratory flow is a passive process so the ratio between expiratory time and expiratory time constant is very important in assessing the respiratory mechanics. After one time constant (or ratio of one between the expiratory time and expiratory time constant), the expiratory flow will decrease by 63.3% to reach a value of 36.7%. The expiratory flow will decrease by 99.3% to reach a value of 0.7% after five time constant (ratio of 5). [VI,XIV] The expiratory flow will not reach the zero reference baseline if the ratio decreases. If the expiratory time is not sufficient then the amount of tidal volume exhaled will be incomplete resulting in trapping of air which is clearly shown in the figure 10. The inhaled tidal volume is the product of constant or average inspiratory flow and inspiratory time. If the inspiratory flow is increased then the required tidal volume is inhaled with a short inspiratory time that will help in increasing the expiratory time. The frequency and total cycle time duration are inversely related. So decreasing the frequency will increase the total cycle time (TCT) duration that may help in increasing the expiratory time depending on I: E ratio. The inspiratory time and expiratory time can be adjusted to maintain a required I: E ratio.

The current research study clearly discussed the derivation and the application of these newly derived modified equations of motion of the respiratory mechanics which are considered as differential equations and not algebraic equations. Some of the parameters in these equations are held constant while others are a variable quantity that changes with changes in other parameters. These novel equations may help in better understanding of the ventilator graphics that play a significant role in management of critically ill patients.

18. CONCLUSION

The ventilator graphics is an indispensable tool that plays a significant role in saving the life of the mechanically ventilated patients. The study concludes that understanding of the various physical concepts involved in mechanical ventilation and the application of these derived modified equations of motion of the respiratory mechanics at the bed side for monitoring these patients may help in better understanding required for the interpretation of invaluable ventilator graphics.

REFERENCES

Application of Modified Derived Equations of Motion of Respiratory Mechanics in the Interpretation of Ventilator Graphics

[12] Stephen E. Lapinsky Auto-PEEP. Encyclopedia of Trauma Care. 2015 DOI: https://doi.org/10.1007/978-3-642-29613-0_234


[14] Paul Ouellet Waveform and loop analysis in Mechanical Ventilation. SIEMENS 1997, Pages 7-84

[15] Charles S. Williams RRT, AE-C VENTILATOR GRAPHICS ver.2.0


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