

Aspects about the Influence of Superficial Heat Treatment on Metal Coating Layers

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Abstract: *Laser heat treatment was applied after coating. Evaluation of results was made by observing the microstructures with metallographic microscopy, SEM/EDX and the mechanical properties were obtained by micro hardness and wear resistance. The goal of this research is to study the influence of the laser heat treatment on wearing resistance of metal coating layers. Results reveal the influence of microstructures and chemical composition of used electrodes on micro hardness and wear resistance of metal coating layers.*

Keywords: *metal coating, laser heat treatment, wearing resistance*

1. INTRODUCTION

The metal coating process is based on the need to protect metal parts and structures from damage by exploitation conditions. Metals used for structural components, mechanisms, enclosures, etc. include steel, stainless steel, aluminum, and titanium. These metals will increase the wear resistance and give the opportunities to recover some components.

Surface treatments made by laser beam irradiation include laser hardening, laser alloying, and laser cladding [1, 2]. The common feature of all of these processes is the production of certain thermal cycles in small, highly localized regions on the surface of the work-piece, which then takes on new properties that allow it to cope better with wear, fatigue, and corrosion while maintaining most of its other original properties [3].

Recent reviews of the principles and applications of laser treatments describe the use of lasers as a controlled heat source for transformation hardening [4]. The classical approach to modeling the heat flow induced by a distributed heat source moving over the surface of a semi-infinite solid starts with the solution for a point source and integrates it over the area of the beam. This widely used method requires numerical procedures for its evaluation, as do the finite difference solutions of Shuja et al. [5]. They developed a 3-D heat flow model and varied the beam power and traverse speed to determine the dimensional analysis of heat flow during heat treating and melting. But the results were not easy discretion of complex shapes and needed complicated calculation. Several authors have used finite-element method for numerical evaluation, as do the FEM analyses of W. Dai and co-workers [6]. The goal of this paper is to make a correlation between the microstructures and the mechanical properties of the metal coating layers after laser heat treatment

2. RESEARCH METHODS

The metal coating was made with arc welding Luftarc 150 Ductil equipment, using four types of electrodes (table 1). The welding current intensity was 700 A, the welding voltage was 40 V, welding velocity 40-45 mm/min. and width of welding bead was 10 mm. The base metal was S275JR SR EN 10025-2:2004, 20 mm thick. The coating layer was 5 mm thick for all the samples. After coating, the samples were annealed at 600°C, to eliminate the internal stresses.

Table 1. *Electrodes used in research*

Electrode	Chemical composition [%]								
	C	Si	Mn	Cr	Ni	Mo	W	P	V
EI CrMn2	0.5-0.7	0.2-0.3	1.5-2.2	10-12					
EI CrW2	0.4-0.6	0.8-1.3	1.5-2.2	0.8-1.2			2.3-3.0		
EICrW8Co	0.3-0.4	0.8-1.3	0.8-1.5	1.3-2.0			7.0-9.0		
E 3161	0.10	0.9	0.5-2.5	17-20	11-14			0.04	

3. RESULTS AND DISCUSSION

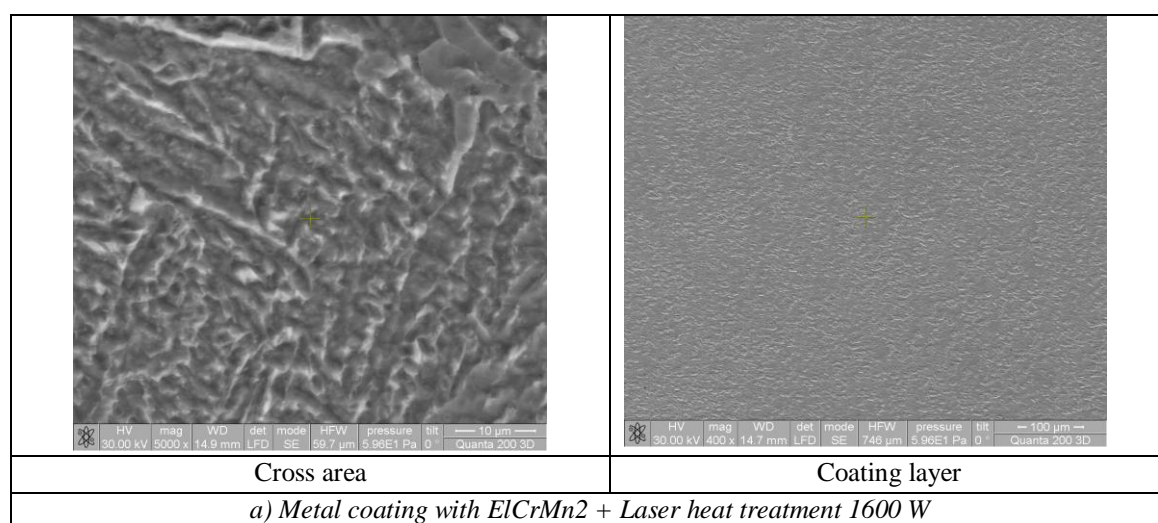
Laser heat treatment was applied on eight types of welding coating layers, presented in table 1. The sample was subject to laser heat treatment in nine variants, with laser source Nd:YAG – Rofin DY 570 Germany, directed with ABB – Sweden robots. Table 2 presents the intensity of laser beam at surface heat treatment, which was choice to cover a large range of laser heat treatments.

Table 2. *Intensity of laser beam and sample notation*

Intensity of laser beam [W]	1400	1500	1600	1700	1875	2150	2425	2600	2700
Electrodes type									
EI CrMn2	[0-1]	[0-2]	[0-3]	[0-4]	[0-5]	[0-6]	[0-7]	[0-8]	[0-9]
EI CrW2	[1-1]	[1-2]	[1-3]	[1-4]	[1-5]	[1-6]	[1-7]	[1-8]	[1-9]
EICrW8Co	[2-1]	[2-2]	[2-3]	[2-4]	[2-5]	[2-6]	[2-7]	[2-8]	[2-9]
E 3161	[E-1]	[E-2]	[E-3]	[E-4]	[E-5]	[E-6]	[E-7]	[E-8]	[E-9]

The results were evaluated with PMT 3 micro-hardness tester, electronically microscope Nova Nano SEM and chemical analyzer EDAX Orbis Micro-XRF.

Laser treated layer thickness is between 0.2 – 0.9 mm, depends on intensity of laser beam. The structures obtained using SEM techniques are presented in figure 1.



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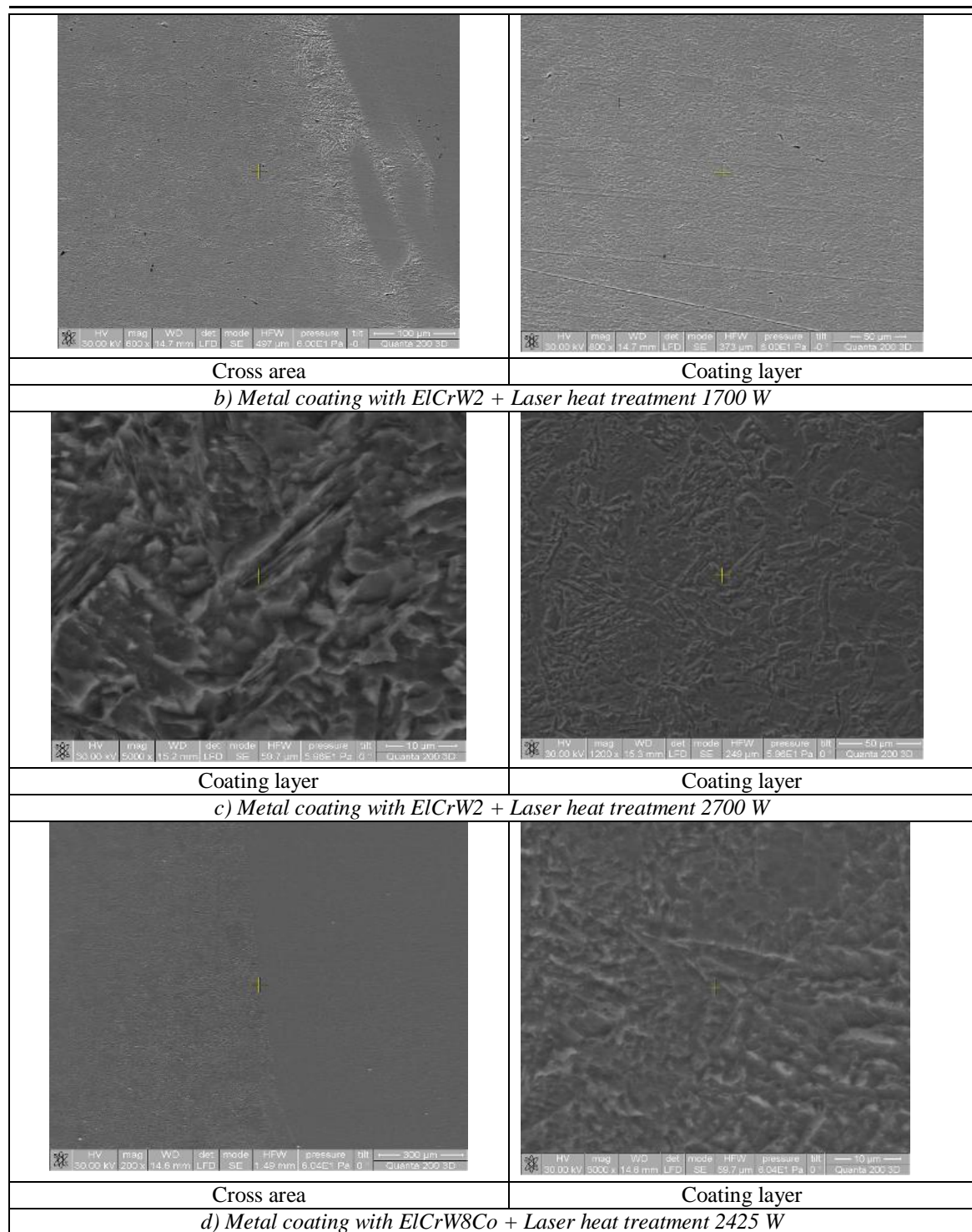


Figure 1. SEM structures of the cross area and the metal coating layers

Studying the microstructures of coated sample with E 3161, which have a low concentration of C, one may observe the ferrite-pearlite structure of base material and weld material structure with martensitic structure having a needle shape. For other five types of electrodes, which have more C, more pearlite structures were obtained. The base material has ferrite-pearlite structures, with lamellar pearlite. Based on the research area, columnar dendrites structures in Fe matrix with good delimitation may be observed.

Increasing the Cr concentration determines the formation of Cr_3C_2 chemical compound in ferrite-pearlite matrix, especially in the case of electrodes CrMn2 and 3161. In the case of metal coating layers with electrodes CrW2, which have low concentration of Cr, the formation of chemical compound cannot be observed.

Evaluation of mechanical properties was made with micro hardness and wear resistance. The obtained micro hardness is presented in figure 2.

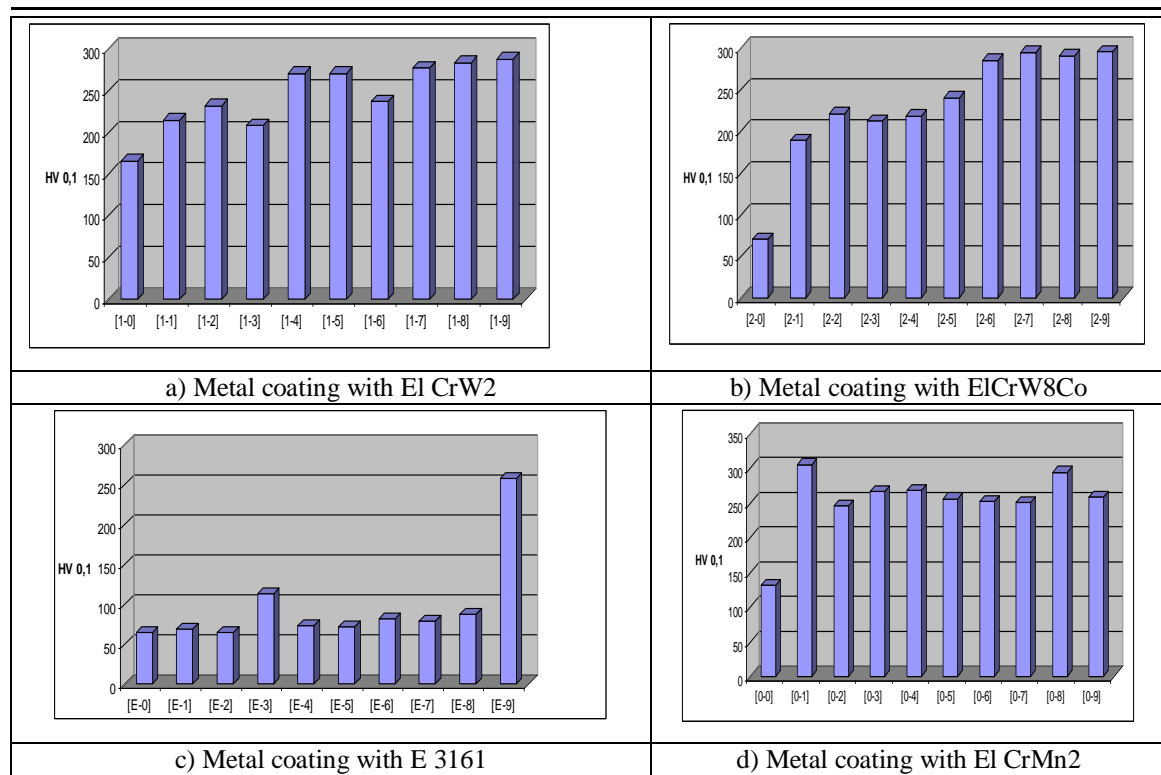


Figure 2. Micro hardness of the metal coating layers

As one may notice from the experimental outcomes, the samples with laser surface heat treatment have a wearing resistance that is mostly superior to the classically thermal treated samples. In the case of laser surface heat treatment layers the existence in combination layer of isolated dot-shaped pores does not significantly influence the hardness of the laser surface heat treatment area or the cohesion with the diffusion sub-layer. It does though allow the enhancement of surface lapping capacity, as a result of lubricant retention in the superficial pores, linked to the surface through channels.

Wear resistance was tested after 15, 30, 60 and 120 minutes of wear and weighing of samples. Determination of weight loss was made with "Oertling - England" balance, accuracy 10^{-2} grams. Results are presented in the wear diagrams, figure 3...6

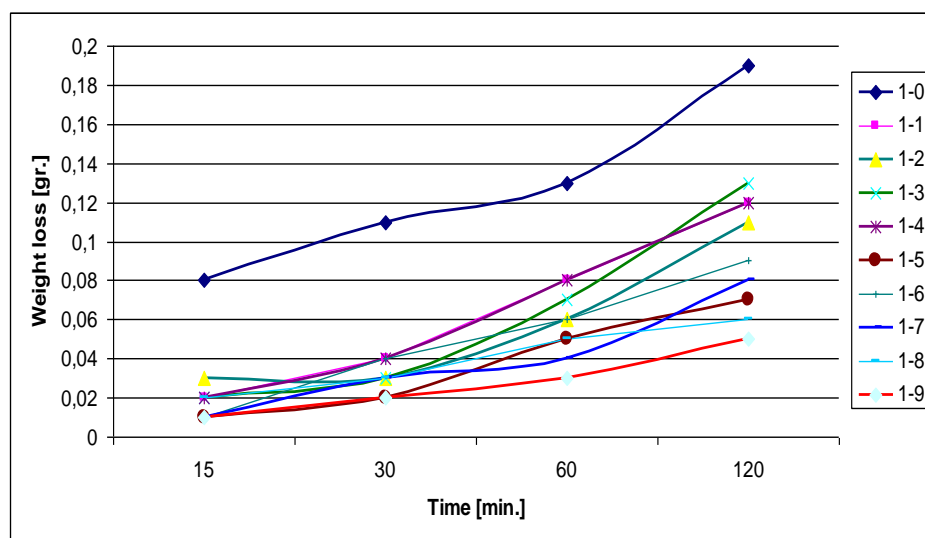


Figure 3. Wear diagrams of metal coating layers Metal coating with EICrW2

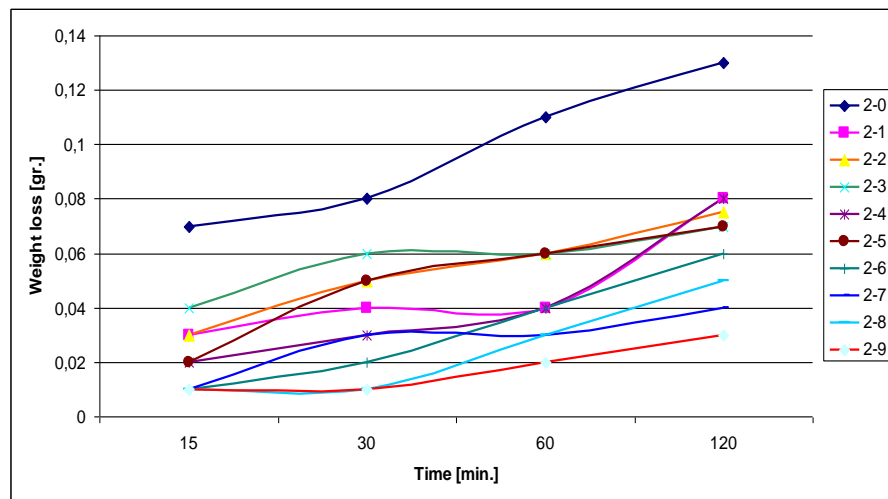


Figure 4. Wear diagrams of metal coating layers Metal coating with EICrW8Co

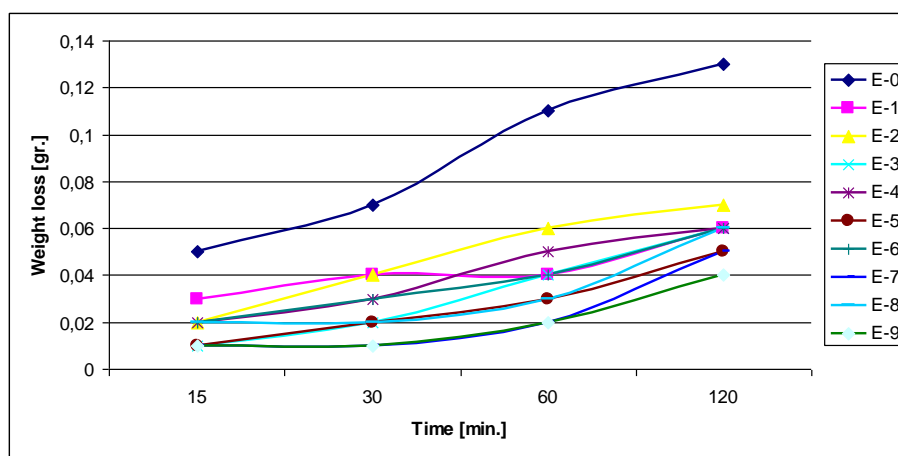


Figure 5. Wear diagrams of metal coating layers Metal coating with E 3161

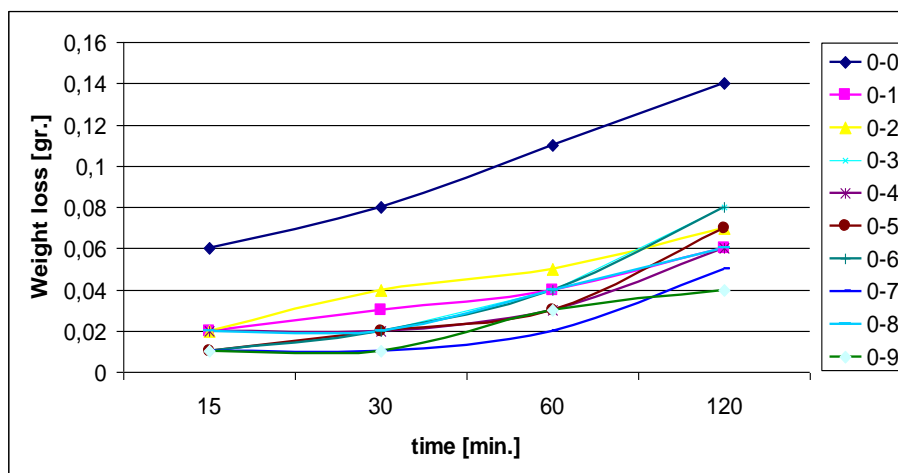


Figure 6. Wear diagrams of metal coating layers Metal coating with CrMn2

4. CONCLUSION

Studying the SEM structures, presented in figure 1, the microhardness (figure 2) and wear resistance (figure 3...6), one may observe a good correlation between the microhardness and wear resistance, increasing the microhardness determinate increase of wear resistance. After the low intensity laser surface heat treatment, that changes the structures of materials, results the partial transformation of ferrite in perlite with higher C concentration, increasing mechanical properties. In case of high intensity of laser surface heat treatment, more than 2000 W, one may observe the

formation of remelted structures, the result being the significantly increase of mechanical properties.

Wear resistance is perhaps the most significant property resulting from this surface treatment. The ability of the compound zone to resist wear is dependent on the type of wear system, specifically whether it is adhesive or abrasive wear. Adhesive wear occurs when two components are in relative motion in an essentially abrasive free environment. Under these conditions, the intrinsic physical characteristics of the compound zone, i.e. hardness and lubrication, notably improve the sliding and running behavior and consequently, increase the resistance to adhesive wear. The phase composition of the compound zone that demonstrates the best wear resistance consists predominantly of epsilon nitride phase (monophasic preferred) with a very small amount of gamma prime phase. Resistance to abrasive wear is dependent on the relative harnesses of the abrading substance and of the compound zone.

The outermost layer identified as the compound zone, and the subjacent interior layer is called the diffusion zone. Each of the zones contribute to improving performance by enhancing specific engineering properties, i.e. wear resistance, lubrication, corrosion resistance, and fatigue strength. From these, other benefits in performance are realized: excellent running properties, anti-galling and anti-seizing characteristics, and reduced tendency for fretting corrosion.

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